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# Applying the SAFEPORT system in a storm situation

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ABSTRACT: This paper presents an application of the SAFEPORT safety system. It consists of a forecast and early warning system for emergency situations related to navigation, berthing, and mooring in port areas. The prototype of the system is being developed for the Port of Sines. The main objective of this paper is to describe the application of the numerical models in SAFEPORT to simulate the behavior of three different ships moored in three terminals of the Port of Sines, subjected to the sea-wave conditions of the Dora storm. The 3-day advance sea-wave forecasts provided by the WAM model were used. Tide levels and currents were obtained from the XTide model. It was concluded that the SAFEPORT system was able to forecast possible hazards and issue the expected alerts regarding the moored ships' motions and the forces on their mooring lines associated to the Dora storm.

#### INTRODUCTION

The significant increase of cargo volume in the Iberian Peninsula as well as the increase in the size of the ships calling at its ports has driven several portexpansion plans. The new ships require deeper vaters, which leads them to be berthed in very exposed locations. In addition, the number of major storms that formed in the Atlantic Ocean reached a new maximum in 2020. The harbors of the Portuguese West coast are exposed to such storms, and this is a key factor for the safety of ships moored there.

In this new scenario, to ensure the efficiency of port operations, as well as the required safety levels during a storm situation, it is important to predict, in dvance, the sea agitation inside the port and its consequences for ships that will enter the port or are berthed and moored inside. Due to the lack of systems duresing the hazards related to ships maneuvering and moored in ports, the SAFEPORT system, based to the HIDRALERTA system (Fortes et al., 2015, 2017, Poserio et al., 2017 and Pinheiro et al., 2020), is considered as part of the BlueSafePort project.

(EWS) for emergency situations related to moring, and berthing in port areas. It protour forecasts of the characteristics of sea to consequences related to ship movements in the mooring systems and the associated levels. A prototype of the SAFEPORT to consequences for the Port of Sines.

This paper presents an application of the SAFE-PORT system, more specifically, the application of the numerical models developed to simulate the behavior of three different ships docked and moored at three terminals of the Port of Sines subjected to the sea-wave conditions of storm Dora, which reached mainland Portugal on December 4<sup>th</sup>, 2020.

To execute the numerical models for wave propagation and moored ship behavior, the safety system, herein presented, uses the integrated numerical tool, SWAMS — Simulation of Wave Action on Moored Ships (Pinheiro *et al.* 2013).

After this introduction, section 2 presents the SAFEPORT system in terms of its operation and numerical models. Section 3 describes the case study, the numerical models used, and the results produced by the SAFEPORT system. Finally, section 5 presents the main conclusions provided by this research.

#### 2 THE SAFEPORT SYSTEM

The SAFEPORT EWS issues daily forecasts for the next 72 hours, at three-hour intervals, of sea agitation within a port and its consequences on ships (in maneuvering or moored).

### 2.1 Methodology

The SAFEPORT safety and alert system, similarly to the HIDRALERTA system (Poseiro, 2019 &

DOI: 10.1201/9781003320289-22

Pinheiro et al., 2020), comprises 4 modules: I - Seawave characterization; II - Navigation in Port Areas; III - Monitoring; IV - Risk Assessment.

The first two modules integrate a set of numerical models. Some models are included in the SWAMS tool (Pinheiro et al. 2013). Those associated with the behavior of maneuvering ships are not included in this work and are carried out by the Centre for Marine Technology and Ocean Engineering (CENTEC). Numerical simulations run on the Central Node for Grid Computing (NCG) of the Portuguese Infrastructure for Distributed Computing (INCD), a 64-node high performance computing facility.

The third module consists of in situ monitoring required to validate the results produced by the numerical models.

The last module deals with risk assessment for moored ships, which is performed through the definition of hazard levels from 0 to 2 for the moored ships' motions and from 0 to 3 for the forces on their mooring lines.

Concerning the moored ships' motions, 0 corresponds to no danger (green symbol), 1 corresponds to a situation of restricted loading and unloading operations (yellow symbol) and 3 corresponds to the maximum warning level (red symbol). The limits imposed on the ships' motions are the recommended ones in PIANC (1995).

As for the forces on ships' mooring lines, the hazard levels depend on the Maximum Breaking Load (MBL) of the mooring lines (OCIMF, 1992). 0 corresponds to no danger (green symbol), 1 corresponds to 50% of MBL (yellow symbol), 2 corresponds to 80% of MBL (orange symbol) and 3 corresponds to 100% of MBL (red symbol).

Figure 1 shows the symbols used in the system to issue alerts.





Figure 1. Symbols used by the SAFEPORT system to alert ships' motions danger (left) and ships' mooring systems failure danger (right).

# 2.2 SWAMS numerical software package

SWAMS (Pinheiro et al. 2013), acronym for Simulation of Wave Action on Moored Ships, is an integrated numerical tool capable of simulating the response of a moored ship within a harbor, subjected to the action of sea waves, wind and currents. This tool consists of a graphical user interface and a set of modules that deal with the execution of numerical models for wave propagation and the behavior of moored ships inside harbor basins.

SWAMS consists of 2 modules (Figure 2): the WAVEPROP module for wave propagation and the MOORNAV module for moored ship behavior. The objective of the first module is to determine the seawave characteristics in the study area. The second module estimates ship movements and the forces exerted on the mooring system.

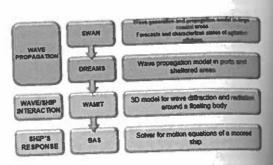


Figure 2. Structure of SWAMS numerical software package used in the case study (adapted from Pinheiro et al., 2013).

The WAVEPROP wave propagation module includes 3 numerical models for wave propagation and a finite element mesh generator, namely:

- SWAN (Booij et al., 1996) is a spectral nonlinear model based on the wave action conservation equation, which simulates the propagation of irregular wave spectrum;
- DREAMS (Fortes, 2002) is a linear finite element model, based on the mild slope equation, to simlate the propagation of monochromatic waves;
- BOUSS-WMH (Pinheiro et al., 2011) a nonlinear finite element model, based on the extended Boussinesq equations deduced Nwogu (1993), being able to simulate the propagation of regular and irregular waves;
- GMALHA (Pinheiro et al., 2008) is a triangular finite element mesh generator specially defined be used by DREAMS and BOUSS-WMH mode being the node density of the meshes variate according to the local wavelength and its constitution optimized to reduce computational resources.

The MOORNAV moored ship behavior modificulties 2 numerical models (Santos, 1994), name

- WAMIT (Korsemeyer et al., 1988) which solve in the frequency domain, the radiation and fraction problems of the interaction a free-floating body and the incident waves.
- BAS (Mynett et al., 1985) that assemble solves, in the time domain, the equation motion of a moored ship, considering the series of forces due to the waves incident on ship, the ship's impulse response functions the constitutive relations of the mooring spelements (mooring lines and fenders).

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ig the time dent on the actions and ring system The numerical model SWAN transfers the wave characteristics from the offshore area to the harbor entrance. The DREAMS model and the BOUSS-WHM model, in turn, transfer the wave characteristics from the harbor entrance area to the harbor area, using the harbor mesh generated by GMALHA. The WAMIT numerical model determines the response of the free-floating ship to incident monochromatic waves. Then, with the hydrodynamic information obtained, it is possible to determine the moored ship response through the BAS numerical model.

### 3 PORT OF SINES CASE STUDY

The Port of Sines is a deep-water port located on the west coast of mainland Portugal (Figure 3). The port has 7 terminals, namely: the Liquid Bulk Terminal (TGL), the Liquified Natural Gas Terminal (TGN), the Petrochemical Terminal (TPQ), the Sines Container Terminal or Terminal XXI (TCS), the Sines Multipurpose Terminal (TMS), the Fishing Port and the Sines Marina.

Given its national relevance, its continuous economic growth and constant expansion, the port of Sines has been the subject of several research projects. The prototype of the SAFEPORT system, for example, has been developed and validated for the Port of Sines. For that, SWAMS (Pinheiro et al. 2013) was employed to simulate the behavior of three different ships docked and moored at three terminals of the Port of Sines subjected to the sea-wave conditions of storm Dora, namely: an oil tanker at the TGL, a general cargo ship at the TMS, and a container ship at the TCS (Figure 3).



Thus, and the TCS.

Storm Dora reached its highest intensity during attended of 4<sup>th</sup> December 2020, and the early December 2020. According to Civil December 2020

height of 10.3 meters at the wave buoy in front of the Port of Sines.

#### 3.1 Basic Data

The 3-day advance forecast of the offshore sea agitation was obtained through the European Centre for Medium-Range Weather Forecasts (ECMWF) (Persson, 2001), which uses the WAM model (WAMDI Group, 1988) used by. The forecasts for 4 and 5 December were collected every 3 hours for the following sea wave parameters: significant wave height  $(H_s)$ , peak wave period  $(T_p)$  and mean wave direction  $(\theta_m)$  (Figure 4).

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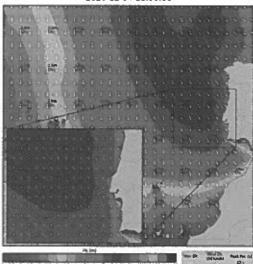


Figure 4. WAM model results offshore the Port of Sines (H<sub>s</sub>, T<sub>p</sub> and  $\theta_m$ ) for 4<sup>th</sup> December 2020, 6 p.m.

The WAM model predicted that the waves formed due to storm Dora would have a predominant  $\theta_m$  of north, with  $H_s$  ranging between 3 and 8 m and a maximum  $T_p$  of approximately 18 s.

The tide levels were estimated with the XTide model (Flater, 1998). Wind data was obtained from the NAVGEM model (Reynolds et al., 2011). Bathymetry was provided by Sines and Algarve Ports Administration. The general geometric characteristics of the ships are shown in Table 1.

Table 1. General geometric characteristics of the simulated ships.

	Draft	Beam	Length overall
Ship	m	m	m
Oil Tanker	22.0	26.5	340
General Cargo	10.5	30.0	220
Container	8.0	19.0	120

# 3.2 Sea-waves propagation and characterization

3.2.1 SWAN numerical model application

The SWAN numerical model (Booij et al., 1996) was applied to propagate the sea agitation parameters, from offshore to the entrance of the port of Sines. The theoretical JONSWAP spectrum was assumed to represent the real spectrum of the waves

approaching the port.

To achieve a better numerical performance, the model domain was discretized into three nested rectangular grids (Figure 5). The physical phenomena accounted by SWAN were diffraction and dissipation by bottom friction. The simulations were performed in the two-dimensional stationary mode. In the third, the smallest, mesh one point was defined, in the vicinity of the port of Sines, where the wave characteristics i.e.,  $H_{\rm s}$ ,  $T_{\rm p}$  and  $\theta_{\rm m}$ , were extracted.

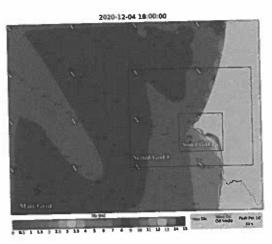


Figure 5. SWAN model results at port of Sines ( $H_e$ ,  $T_p$  and  $\theta_m$ ) for 4<sup>th</sup> December 2020, 6 p.m. PO stands for the North offshore point of the WAM model and PE stands for the transfer point from SWAN to DREAMS.

On the 1st day of the storm, the observed waves in front of the port had their  $T_p$  between 15 s and 17 s, and  $H_s$  between 3 m and 7.55 m (maximum Hs occurred at 6 p.m.). The most frequent situation corresponds to  $H_s$  between 6 m and 6.5 m. As for  $\theta_m$ . Northwest incidences represent the predominant direction of the waves. For the  $2^{nd}$  day of storm Dora, the sea agitation conditions were less severe. A maximum  $H_s$  of 6.94 m was obtained at 12 a.m. with a  $T_p$  of 15.09 s. The predominant  $\theta_m$  was also northwest.

# 3.3 DREAMS numerical model application

The DREAMS model simulates the propagation of monochromatic waves on gently sloping bottoms, considering the combined effects of refraction, diffraction and partial or total reflection of the port area boundaries.

To do the modelling, a finite element mesh generated by GMALHA (Pinheiro et al., 2008) was used to characterize the morphology of the Sines harbor. In addition, a file containing information about the absorption coefficients of each section of the port boundary was assigned to the model. Results (Figure 6 and Figure 7) were extracted at three points near the three terminals where the ships' behavior was simulated.

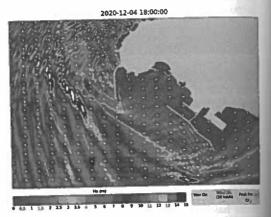


Figure 6. DREAMS model results at port of Sines (significant wave height and mean wave direction) for 4<sup>th</sup> December 2020, 6 p.m. PE stands for the transfer point from SWAN to DREAMS.

Sea waves approach the TGL with  $\theta_m$  from south to southwest and  $H_s$  ranging between 0.1 m and 1.2 m. The peak was recorded at 9 p.m., on December- $4^{th}$ , with  $H_s = 1.2$  m,  $T_p = 15$  s and  $\theta_m = 210^{\circ}$ .

The TMS, in turn, is affected by waves coming from the west with H<sub>s</sub> not exceeding 0.7 m. The peak occurred at 6 p.m., on December 4<sup>th</sup>, with H<sub>s</sub>=

0.7 m,  $T_p = 15 \text{ s and } \theta_m = 280^\circ$ .

Finally, at the container terminal, the incident wave action was characterized by south swells with Hs ranging from 0.12 m to 0.84 m. The peak occurred at 3 a.m., with  $H_s = 0.8$  m,  $T_p = 1.7$  s and  $\theta_m = 1.74^\circ$ . Although wave heights offshore ( $H_s \sim 4$  m) were not close to the highest recorded (at 6 p.m. on December  $4^{th}$ ), the waves rotating slightly to the west led to the largest impact inside the port.

## 3.4 Behavior of the moored ships

3.4.1 WAMIT numerical model application
The WAMIT model (Korsemeyer et al., 1988) was applied to calculate the hydrodynamic coefficients the free ships, i.e., the damping and added-mass coefficients. For this purpose, one needs the geometry the submerged hulls discretized into rectangular angular flat panels and the mass distribution (inertial of the ships. The submerged hull of the oil tanks was

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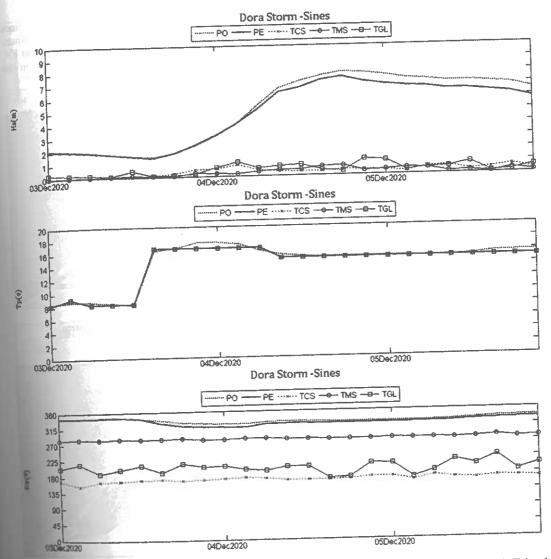


Figure 7. DREAMS model results at each terminal of the port of Sines (significant wave height (Hs), period peak (Tp) and mean wave direction (Dir)). PO stands for the North offshore point of the WAM model and PE stands for the transfer point from SWAN to DREAMS.

discretized with 1004 panels, the general cargo ship with 1992 panels and the container ship with 3464 panels (Figure 8). The tool used was NPP, acronym tor Nautical Pre-Processor (Santos, 1994).

The WAMIT simulations were performed for the wave directions approaching each terminal and a range of 89 frequencies. Once the damping officients of the ships were computed, the impulse functions (Figure 9) were obtained. The frequency added masses were estimated and on the corresponding frequency domain added mass values for a given frequency and on the corresponding retardation functions.

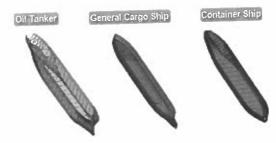


Figure 8. Panel discretization for the 3 ships.

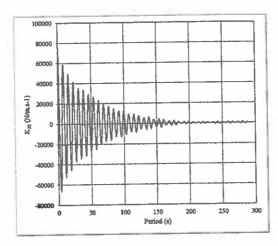


Figure 9. Impulse response (top) and infinite frequency added-mass (bottom) of the general cargo ship for the motion mode j, k = 2, 2.

3.4.2 BAS numerical model application

The application of the BAS model (Mynett et al., 1985) to the moored ships allows one to obtain the motion of these ships and the forces in their mooring systems. As input parameters, in addition to the sea wave conditions, the BAS model used the information computed by the WAMIT model, the coordinates of the mooring points and the coordinates of the contact points between the ships and the fenders.

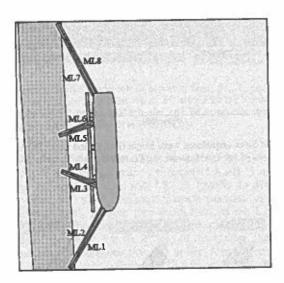


Figure 10. Oil tanker ship mooring system.

For the oil tanker and the general cargo ship, 8 mooring lines grouped in two and 3 fenders were defined (Figure 10 and Figure 11). For the container ship model, a total of 10 mooring lines and 5 fenders were defined (Figure 12).

The constitutive relations for all the mooring lines are linear. For an elongation of 4%, the maximum load on mooring lines of the oil tanker is 2100 kN, on the general cargo ship is 1900 kN and, on the container is 1860 kN.

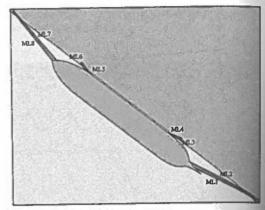


Figure 11. General cargo ship mooring system.

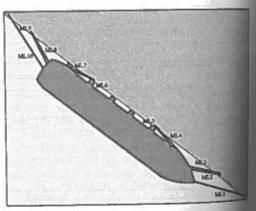


Figure 12. Container ship mooring system.

The same constitutive relations were considered to the oil tanker and the general cargo ships' fenders non-linear range from 0 kN to 880 kN maximum with a maximum deflection of 0.4 m. As for the tainer ship, its fenders have a linear compression a maximum force of 8900 kN for a deflection of maximum

## 4 RESULTS AND DISCUSSION

Sea wave results provided by the WAM and SWA models show that at 6 p.m. on December 4 corresponds to the most critical time of storm December, according to the DREAMS model within the port, i.e., in the vicinity of the terms under study, the storm peaks occurred at different times (Figure 7).

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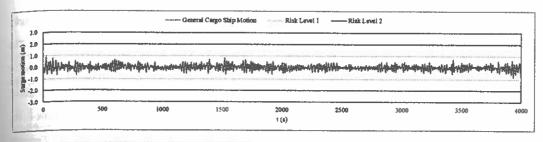


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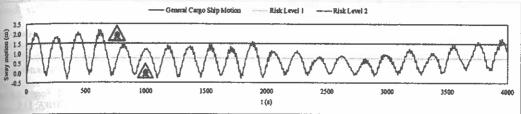


Figure 13. General Cargo Ship's surge and sway motions alerts.

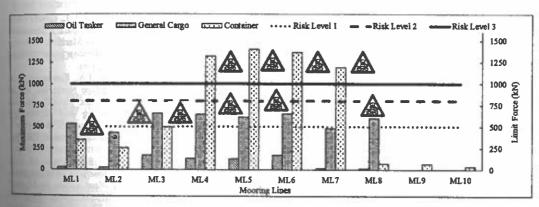


Figure 14. Forces on the ships' mooring lines alerts.

To comply with the objectives of the SAFE-PORT system, the ships' motions and the forces on their mooring lines were analyzed, considering the storm peak recorded in the vicinity of the terminals where they are docked. Thus, Figure 13 presents some results for the general cargo ship (ship motions), at 6 p.m., on December 4<sup>th</sup>, obtained by the SAFEPORT system. Figure 14 displays the forces on the ships' mooring lines at the time when the peak occurred.

During storm Dora, no alerts were issued concerning the oil tanker moored at the liquid bulk terminal Despite being the most exposed ship, given to large displacement, no excessive motions of the hip were forecast and, consequently, the forces on the mooring lines are not expected to reach the max-

As for the general cargo ship moored at the multipage terminal, yellow and red alerts (danger level 1 12, respectively) were issued to sway and heave motions. 6 yellow alerts, i.e., danger level 2, were issued to mooring lines 1, 3, 4, 5, 6 and 8. The mooring lines received a maximum load of more than 500 kN. For the others no alerts were issued. This is an expected result, since among the 3 terminals, the TMS is the most protected from sea waves.

The container ship docked at the container terminal was the most affected ship by the storm Dora. Therefore, the system issued 2 red alerts to surge and sway motions, and 1 yellow alert to heave motions. 4 yellow alerts, i.e., danger level 2, to mooring lines 4, 5, 6 and 7. They were exposed to a maximum load of more than 1000 kN. No alerts were issued for the remaining lines.

### 5 CONCLUSIONS

The SAFEPORT system is intended to predict, alert, and assess the occurrence, 72 hours in advance, of

emergency situations associated with the safety of moored ships. To this end, it is essential that the system operates properly in current and storm situations.

This research is part of the SAFEPORT system testing phase. The performance of the system in a storm situation was tested. The developments made to date consist of the application of the prototype developed for the port of Sines in the simulation of the impact of storm Dora on three ships moored at different terminals of the port.

The alerts issued by the system were in accordance with the reported occurrences. It should be noted that these are only preliminary results, as the system is still being validated and tested.

The SAFEPORT system proved to be a useful tool in managing the safety of ships moored in the port of Sines during storm Dora. To ensure that the system provides consistent and reliable information in any situation, further tests and in-depth validation with buoy data are under development.

### **ACKNOWLEDGEMENTS**

The authors would like to thank the BlueSafePort project (ref: FA\_04\_2017\_016), the National Infrastructure for Distributed Computing (INCD) for granting access to the digital infrastructure to support research and the Sines and Algarve Ports Administration.

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